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Rectangular waveguide to coaxial line transition scheme. Parameter w h L d h1 h2 c Value [mm] 10 5 30 2 5 11 9 19.6 Rectangular waveguide to coaxial line transition parameters. The input port is placed at the waveguide and it excites the fundamental TE10 mode and the output port with TEM mode is placed at the coaxial line. Fundamental TE10 mode at the input port. S-Parameters S-Parameters calculated for rectangular waveguide to coaxial line transition. The obtained S-Parameters results indicated that our waveguide-to-coax transition is far from ideal design. There are relatively big reflections over most of the considered band and at the frequency f=20.65 A`2A`2AGHz there is a total reflection. Before changing the design we may wish to know more about what caused such a reflection. Field distribution in the steady state at this frequency may be very helpful here. To obtain such a distribution we should change the waveform of the exciting signal to sinusoidal at 20.65 GHz. Display of Ez field in the envelope mode for the structure at 20.65 A`2A`2AGHz. Even a brief look at the envelope brings the conclusion that at the frequency 20.65 A`2A`2AGHz we have a pure standing wave in the structure and that the reason for this standing wave is the transformation of the waveguide back short over a half-wavelength section to the coax output. Thus the coax output is effectively short-circuited and cannot receive energy from the waveguide. With the above conclusions we know that we need to modify the geometry of the transition and that we need to start by moving the coax output closer to the waveguide short. Modified rectangular waveguide to coaxial line transition. Parameter w h L d h1 h2 c Value [mm] 10 5 30 2 5 11.2 9 25 Rectangular waveguide to coaxial line transition modified parameters. After modifying geometry parameters according to the yna YLPMI ton seodceller orez taht etont eton sla su tel .gnisercni noitces eht Fo htgnel eht htiw orez dnet tsum [11s] sselnoitceller the solnoitcefers of the noitces gnol a ffitotuc eht selnoleb neyve esuaceb siht. [11S] FO Esaerced Tsaf A Osla ni Ereht ,Evitutni ssel mees yam tahw tub .ycneuerf eht FO Esaerced htw TSPord [12S] Ylarututan .ycneuerf ffitotuc eht woleb [12S] DNA [11S] FO seulav eht because cool resolc evah su tel.ycneuerf eht ot lanoitroporp yllarutan si [2Mag] Tuptuo also eht ta elhw .)zhg 51(ffitotuc edugevaw eht because 0 ot spord tnatsnoc noitaporp eht |tupni edugevaw(1 trop taht nees eb detanms simsims of 1 strop simsims eht etoned [2maG] dna [1maG] .zHG A`2A`2AGHz`03 ot 01 morf dnab ycneuerf rediw a ni noitisnart enil laixaoc ot edugevaw ralugnatcer deifdom rof detaluciac sretemaraP-S .rewols scitsiretcarahc lanif eht ot ecnegrevnoc eht ekam dna sessecorp gniyaced ylwols eticxe htoB .fflotuc edugevaw eht woleb osla dna |zHG A`2A`2AGHz`72 tuoba(ycneuerf tnanoser rehghi a ta tiucri eht eticxe ew dnab ycneuerf rediw a htiW .zHG A`2A`2AGHz`03 ot zHG 01 morf dnab ycneuerf rediw a htiw erutcurts eht eticxe won lliw eW ycneuerf ffituc eht woleb sretemaraP-S .zHG A`2A`2AGHz`52.71 ta erutcurts deifdom eht rof edom epolevne eht ni dleif zE fo yalpsiD .snoitceller yna yb debrutrep ton si tupni edugevaw eht ta hci|hw .evaw gnillevert ylerup a gnitartsulli egami eht niatbo eW .ycn euqerf denoitemerofa ta noitaitcxe ladiosunis a htiw erutcurts deifdom eht fo noitalumis eht nur ot yrt won su teL .noitisnart enil laixaoc ot edugevaw ralugnatcer deifdom rof detaluciac sretemaraP-S .zHG A`2A`2AGHz`52.71 ta orez ot esolc snoitceller evah ew .elpmaxe rof .taht Dna devpmi yiraalc Sah noitisnart eht fo ecnamrofrep eht taht Ees nac ew .|zhg A`2A`52-2F DNA ZHG A`2A`11a|F htiw htiw htiw htiwps slumatics. of a real power in the guide since the characteristic impedance of the guide (equal to the reference impedance for the definition of S-parameter) is imaginary below the cutting frequency. The list of all parameters that can be calculated below the cutting frequency is given in cutting calculations below. Parameters S extended In some specific applications, the user may require additional information about the phase angle of the propagation constant and about changes in the characteristic impedances of the port lines (which are also reference impedances for the calculated S-matrix). To extract this extended information, we need to activate Extended Results. Parameters S extended calculated for modified rectangular waveguide for coaxial line transition in a wider frequency band from 10 to 30 GHz. Taking advantage of this functionality, let us notice for this case considered (see results above) that at TEM output we have a constant and real impedance throughout the frequency band. In the wave guide input the impedance is real (

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